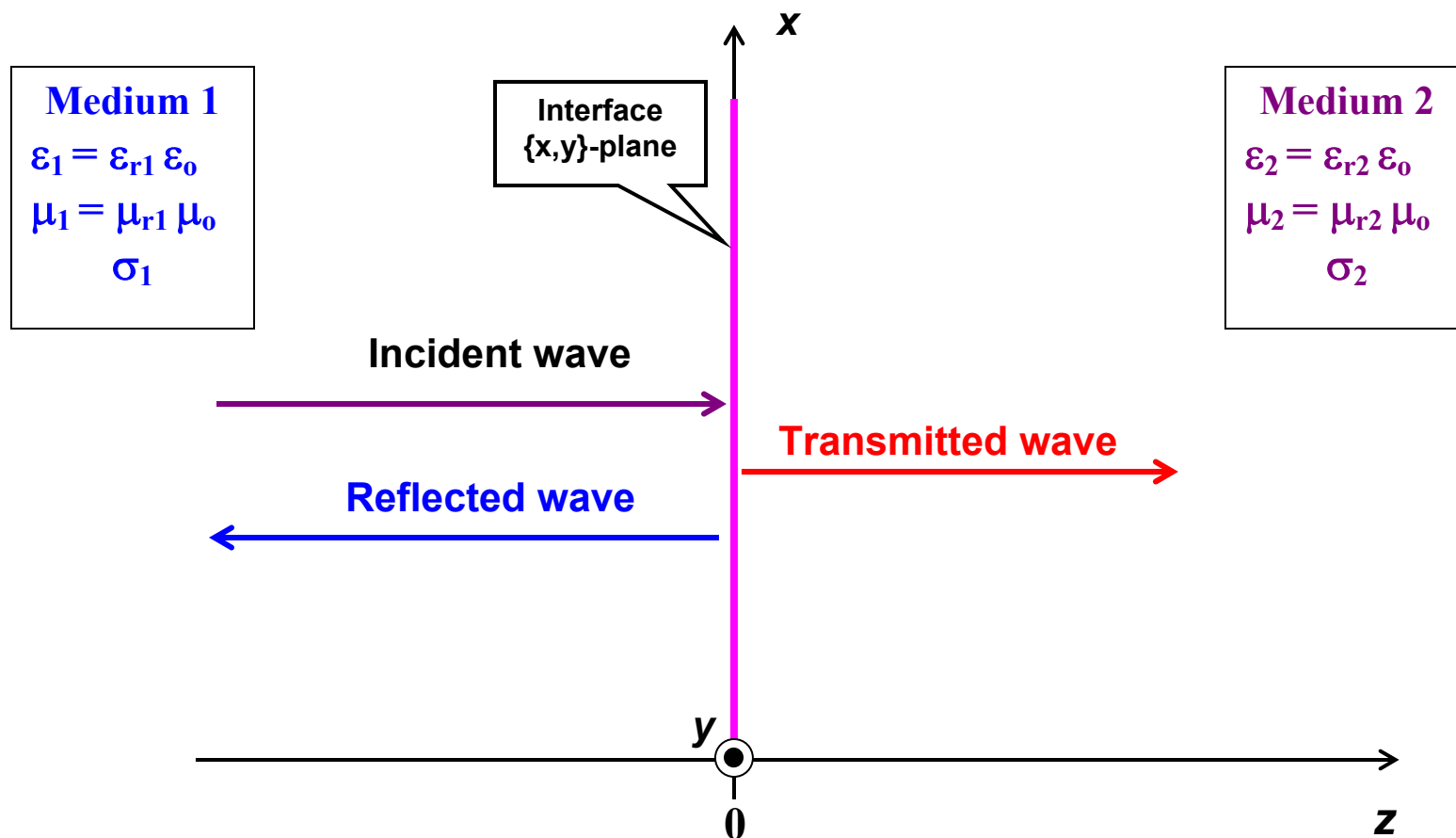


Normal Incidence on an Interface

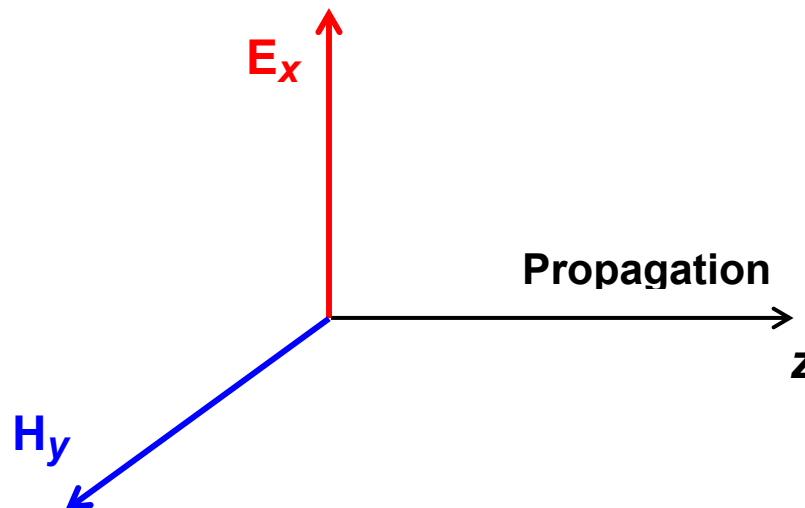
Consider a **planar interface** between two unbounded media, and a uniform plane wave with normal incidence on the interface.



Because of the **medium discontinuity**, the incident wave experiences a partial **reflection** at the interface.

In **medium 2**, only a **forward transmitted wave** exists

The **total fields** at the interface must satisfy the **boundary conditions** for electromagnetic fields. Without loss of generality, we assume the following orientation for the **electromagnetic fields** of the **waves**



Recalling the solution for **Helmholtz equation**, the phasor fields in the **medium 1** can be written as

$$\mathbf{E}_1(z) = \mathbf{E}_1^+ \exp(-\gamma_1 z) + \mathbf{E}_1^- \exp(\gamma_1 z)$$

$$\begin{aligned} \mathbf{H}_1(z) &= \mathbf{H}_1^+ \exp(-\gamma_1 z) + \mathbf{H}_1^- \exp(\gamma_1 z) \\ &= \frac{1}{\eta_1} \left(\mathbf{E}_1^+ \exp(-\gamma_1 z) - \mathbf{E}_1^- \exp(\gamma_1 z) \right) \end{aligned}$$

**Total
Field**

Incident wave

Reflected wave

$$\gamma_1 = \sqrt{j\omega\mu_1(\sigma_1 + j\omega\varepsilon_1)} \quad \eta_1 = \sqrt{\frac{j\omega\mu_1}{\sigma_1 + j\omega\varepsilon_1}}$$

The **forward transmitted wave** in medium 2 is given by

$$\mathbf{E}_{2x}(z) = \mathbf{E}_2^+ \exp(-\gamma_2 z)$$

$$\mathbf{H}_{2y}(z) = \mathbf{H}_2^+ \exp(-\gamma_2 z)$$

$$= \frac{1}{\eta_2} \mathbf{E}_2^+ \exp(-\gamma_2 z)$$

**Total
Field**

Transmitted wave

$$\gamma_2 = \sqrt{j\omega\mu_2(\sigma_2 + j\omega\epsilon_2)} \quad \eta_2 = \sqrt{\frac{j\omega\mu_2}{\sigma_2 + j\omega\epsilon_2}}$$

Both fields are **parallel** to the interface. The boundary conditions indicate that the **total fields** are **continuous** at the interface. Note that we are assuming a **finite conductivity**, therefore **no surface current** exists and the tangent magnetic field is also continuous.

The interface is located at $z = 0$ so all exponentials are equal to 1:

$$\mathbf{E}_{1x}(z = 0) = \mathbf{E}_{2x}(z = 0) \quad \Rightarrow \quad \mathbf{E}_1^+ + \mathbf{E}_1^- = \mathbf{E}_2^+$$

$$\mathbf{H}_{1y}(z = 0) = \mathbf{H}_{2y}(z = 0) \quad \Rightarrow \quad \frac{1}{\eta_1} (\mathbf{E}_1^+ - \mathbf{E}_1^-) = \frac{1}{\eta_2} \mathbf{E}_2^+$$

Assuming that the amplitude \mathbf{E}_1^+ of the incident wave is known, we have two unknowns \mathbf{E}_1^- and \mathbf{E}_2^+ . In order to obtain a general result, it is convenient to solve the equations above in terms of **reflection coefficient** ($\mathbf{E}_1^-/\mathbf{E}_1^+$) and **transmission coefficient** ($\mathbf{E}_2^+/\mathbf{E}_1^+$).

Reflection Coefficient

$$\Gamma_{\mathbf{E}} = \frac{\mathbf{E}_1^-}{\mathbf{E}_1^+} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

This is similar to the voltage load reflection coefficient found for a transmission line, if one considers the following analogy

Medium 1 \Leftrightarrow **Transmission Line**

η_1 \Leftrightarrow Z_0 **Characteristic Impedance**

Medium 2 \Leftrightarrow **Load**

η_2 \Leftrightarrow Z_R **Load Impedance**

For the magnetic field

$$\Gamma_{\mathbf{H}} = \frac{\mathbf{H}_1^-}{\mathbf{H}_1^+} = \frac{-\mathbf{E}_1^- / \eta_1}{\mathbf{E}_1^+ / \eta_1} = -\frac{\mathbf{E}_1^-}{\mathbf{E}_1^+} = -\Gamma_{\mathbf{E}}$$

Transmission Coefficient

$$\begin{aligned}\tau_{\mathbf{E}} &= \frac{\mathbf{E}_2^+}{\mathbf{E}_1^+} = \frac{\mathbf{E}_1^+ + \mathbf{E}_1^-}{\mathbf{E}_1^+} = 1 + \frac{\mathbf{E}_1^-}{\mathbf{E}_1^+} \\ &= 1 + \Gamma_{\mathbf{E}} = \frac{2\eta_2}{\eta_2 + \eta_1}\end{aligned}$$

For the magnetic field we have

$$\tau_{\mathbf{H}} = \frac{\mathbf{H}_2^+}{\mathbf{H}_1^+} = \frac{\mathbf{H}_1^+ + \mathbf{H}_1^-}{\mathbf{H}_1^+} = 1 + \frac{\mathbf{H}_1^-}{\mathbf{H}_1^+} = 1 - \frac{\mathbf{E}_1^-}{\mathbf{E}_1^+} = 1 - \Gamma_{\mathbf{E}}$$

NOTE: The **reflection** and **transmission** coefficients for the **fields** are in general **complex** quantities.

Special cases

Matched Impedances

$$\eta_1 = \eta_2 \Rightarrow \Gamma_{\mathbf{E}} = \mathbf{0} \quad \text{and} \quad \tau_{\mathbf{E}} = \mathbf{1}$$

In this case we have **total transmission** into medium 2 and no reflection.

Medium 2 = Perfect Conductor

$$\sigma_2 \rightarrow \infty \Rightarrow \eta_2 = \mathbf{0} \Rightarrow \Gamma_{\mathbf{E}} = -\mathbf{1} \quad \text{and} \quad \tau_{\mathbf{E}} = \mathbf{0}$$

The wave experiences **total reflection**, consistent with the fact that the fields must be zero inside the perfect conducting medium. This case is analogous to a line with a short circuit load. The total electric fields at the interface is

$$\mathbf{E}_1^+ + \mathbf{E}_1^- = \mathbf{E}_1^+ + \Gamma_{\mathbf{E}} \mathbf{E}_1^+ = \mathbf{E}_1^+ - \mathbf{E}_1^+ = \mathbf{E}_2^+ = \mathbf{0}$$

Perfect Dielectric Media

$$\sigma_1 = 0 \Rightarrow \eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} = \mathbf{Real}$$

$$\sigma_2 = 0 \Rightarrow \eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \mathbf{Real}$$

Usually,

$$\mu_1 = \mu_2 = \mu_0$$

$$\Rightarrow \Gamma_E = \frac{\sqrt{\mu_0 / \epsilon_2} - \sqrt{\mu_0 / \epsilon_1}}{\sqrt{\mu_0 / \epsilon_2} + \sqrt{\mu_0 / \epsilon_1}} = \frac{1 - \sqrt{\epsilon_2 / \epsilon_1}}{1 + \sqrt{\epsilon_2 / \epsilon_1}} = \mathbf{Real}$$

$$\tau_E = 1 + \Gamma = 1 + \frac{1 - \sqrt{\epsilon_2 / \epsilon_1}}{1 + \sqrt{\epsilon_2 / \epsilon_1}} = \frac{2}{1 + \sqrt{\epsilon_2 / \epsilon_1}} = \mathbf{Real}$$

Power flow

Assuming dielectric media (no-loss) for simplicity, the **time-average power** associated with the incident wave and the reflected wave is

$$\langle \vec{P}(t) \rangle_{in} = \frac{1}{2} \operatorname{Re} \left\{ \vec{E} \times \vec{H}^* \right\} = \frac{1}{2} \frac{|\mathbf{E}_1^+|^2}{\eta_1}$$

$$\langle \vec{P}(t) \rangle_{refl} = \frac{1}{2} \frac{|\mathbf{E}_1^+|^2}{\eta_1} |\Gamma_E|^2$$

The power reflection coefficient is

$$\Gamma_P = \frac{\langle \vec{P}(t) \rangle_{refl}}{\langle \vec{P}(t) \rangle_{in}} = |\Gamma_E|^2$$

The time-average power flow **transmitted** in **medium 2** is

$$\langle \vec{P}(t) \rangle_{trans} = \frac{1}{2} \frac{|E_2^+|^2}{\eta_2}$$

Also

$$\langle \vec{P}(t) \rangle_{trans} = \langle \vec{P}(t) \rangle_{in} - \langle \vec{P}(t) \rangle_{refl} = \frac{1}{2} \frac{|E_1^+|^2}{\eta_1} (1 - |\Gamma_E|^2)$$

since power flow **normal** to the interface must be **continuous**

$$\Rightarrow \frac{1}{2} \frac{|E_2^+|^2}{\eta_2} = \frac{1}{2} \frac{|E_1^+|^2}{\eta_1} (1 - |\Gamma_E|^2)$$

The power **transmission coefficient** is

$$\begin{aligned}\tau_{\mathbf{P}} &= \frac{\langle \vec{P}(t) \rangle_{trans}}{\langle \vec{P}(t) \rangle_{in}} = |\tau_{\mathbf{E}}|^2 \frac{\eta_1}{\eta_2} \\ &= \frac{\langle \vec{P}(t) \rangle_{in} - \langle \vec{P}(t) \rangle_{refl}}{\langle \vec{P}(t) \rangle_{in}} = 1 - |\Gamma_{\mathbf{E}}|^2\end{aligned}$$

Note that, as a consequence of **power conservation**, from the results above one gets

$$\Gamma_{\mathbf{P}} + \tau_{\mathbf{P}} = |\Gamma_{\mathbf{E}}|^2 + 1 - |\Gamma_{\mathbf{E}}|^2 = 1$$

NOTE: the **reflection** and **transmission** coefficients for the **time-average power flow** are always **real**.